

## ANTENNA THEORY

Symbols:

$\Pi$     $\cong$     $\alpha$     $\phi$     $\lambda$     $\leq$     $\neq$     $\geq$     $\pm$     $\theta$     $\Omega$

Circumference of a circle =  $2\Pi r$

Surface of sphere =  $4\Pi r^2$

Volume =  $(4/3)\Pi r^3$

E = volts/m

H = A/m

S =  $W/m^2$  = power density

Impedance of free space = 377 ohms

G = gain ratio =  $P_2/P_1 = 10^{(GdB/10)}$

GdB =  $10 \log (P_2/P_1)$

DBic = circular polarization; dBid =  $dB_i + 2.2$  = reference to a dipole

Fuel vapor hazard =  $S = 5W/cm^2 = 50,000W/m^2 = 5,000mW/cm^2$  [using peak power]

For **3dB**,  $G = 2 = 10^{0.3}$  = surface of sphere/surface of hemisphere =  $(4\Pi r^2) / (2\Pi r^2)$

$S = (\text{power density at distance } r) = PG / (4\Pi r^2)$

$$S = E^2/377 = 377 H^2$$

**Note:**  $PG / (4\Pi r^2)$  represents the **maximum S** for aperture antennas (i.e. the near field requires a gain reduction).

$Gr = 4\Pi Ar/\lambda^2$  ; therefore,  $Ar = Gr\lambda^2/4\Pi$  = the effective aperture area of the receive antenna

$$S = PGt / (4\Pi r^2) = W/m^2$$

$$\text{So, } S(Ar) = (W/m^2)m^2 = W = PtGtGr\lambda^2 / (4\Pi^2)(r^2) = Pr$$

And  $Pr/Pt = GtGr\lambda^2 / (4\Pi^2)(r^2)$  which is a unitless expression.

And  $10\log Pr - 10\log Pt = Gt + Gr + 20\log\lambda - 20\log 4\Pi - 20\log r$  {Note: Gt & Gr are now in dB}

$$\text{So } Pr = Pt + Gt + Gr + 20\log\lambda - 20\log 4\Pi - 20\log r$$

{Note: **10logP = dBW**, referenced to 1W. However, **10log1000P = dBm**, referenced to 1mW. }

Since  $c = f\lambda$  and  $\lambda = c/f$  and  $\lambda^2 = c^2/f^2$

$$Pr = Pt + Gt + Gr + 20\log(c) - 20\log(f) - 20\log(4\pi) - 20\log(r)$$

$$\text{Or } Pr = Pt + Gt + Gr + 20\log(c) - 20\log(f \text{ MHz}) - 20\log(10^{16}) - 20\log(4\pi) - 20\log(r)$$

$$Pr = Pt + Gt + Gr + 169.5 - 20\log(f \text{ MHz}) - 120 - 22 - 20\log(r)$$

$$Pr = 27.5 + Pt + Gt + Gr - 20\log(f \text{ MHz}) - 20\log(r) \quad \{r = \text{meters, } P = \text{dBW or dBm, } f = \text{MHz}\}$$

$$Pr = 37.82 + Pt + Gt + Gr - 20\log(f \text{ MHz}) - 20\log(r) \quad \{r = \text{feet} * 0.3048\text{m/ft}\}$$

$$Pr = -36.6 + Pt + Gt + Gr - 20\log(f \text{ MHz}) - 20\log(r) \quad \{r = \text{miles} * 1609.3\text{m/mile}\}$$

$$Pr = -32.5 + Pt + Gt + Gr - 20\log(f \text{ MHz}) - 20\log(r) \quad \{r = \text{km} * 0.001\text{m/km}\}$$

**TCAS:** TX at 1030 MHz; RX at 1090 MHz.

Maximum ERP =  $Pt * Gt = TRP(360/BW) = 400W = 56 \text{ dBm}$ .

**L-Band Satcom:** TX at 1626.5 – 1646.5 MHz with 5kHz channel spacing.

RX at 1530.0 – 1545.0 MHz (Inm-C) & 1575.42 MHz (GPS).

ERPmax = 16dBW = 46dBm = 39.8W ~ 40W (~20W with 3dB gain).

VSWR ≤ 1.5:1; Z = 50Ω; polarization = RHCP

G =

**IFF:** TX at 1090 MHz; RX at 1030 MHz.

Peak pulse power at transponder =  $27 \pm 3 \text{ dBW} = 30 \text{ dBW max} = 1000 \text{ W} = 60\text{dBm}$

Gt max = 0 dB (includes line loss)

**GPS:** L1 = 1575.42 MHz; L2 = 1227.6 MHz

Gr = -1.0 dBic angles between 0 deg & 75 deg from vertical; -7.5dBic @horizon.

Antenna out-of-band rejection is: >6dB @ 1177 MHz, >10dB @ 1277, >20db @ 1525, >25dB @ 1625 MHz. [These are approximately L1 & L2 +/- 50 MHz]

Antenna VSWR ≤ 2.0 to 1.

Preamp gain = 22-38dB at L1 & L2; filter rejection = 1dB at carrier +/- 15MHz, 3dB at +/- 60MHz, 50db at +/- 100MHz.

**Out-of-Band Interference:** GPS shall handle 0 dBm continuous RF power applied to preamp without degradation of performance for interference outside L1 & L2 bandwidths of ± 100 MHz and from 50 to 12000 MHz (50MHz- 12GHz). [ 50 – 1127.6 and 1327.6 – 1475.42 and 1675.42 – 12000 MHz ]

Gp = spread spectrum processing gain = code rate/data rate.

Therefore C/A code Gp = 1MHz/50Hz = 20,000 = 43dB; p-code Gp = 10MHz/50Hz = 200,000 = 53dB.

**Burnout Level:** At L1 & L2, unit can sustain 10dBm, CW, applied to preamp input for 1minute without damage. Outside L1 & L2 ± 100MHz, unit can sustain 3W(34.77 dBm), CW, applied to preamp input for 1 minute without damage.

**Upper IFF vs GPS Analysis:** IFF location = FS 513; GPS locations = FS 623 & FS 653.

Separation distance =  $623 - 513 = 110 \text{ in}/12 = 9.17 \text{ ft}$

**$Pr = 37.82 + Pt + Gt + Gr - 20\log(f \text{ MHz}) - 20\log(r)$**  {r = feet \*0.3048m/ft}

$Pr = 37.82 + 60 \text{ dBm} + 0 - 7.5 - 20\log(1090) - 20\log(9.17)$

$= 97.82 - 7.5 - 60.75 - 19.25 = \mathbf{10.32 \text{ dBm}}$

However antenna out-of-band rejection is >6dB, and polarization mismatch is -3dB.

Therefore,  $10.32 - 9 \text{ dB} = \mathbf{1.32\text{dBm}}$  which is slightly above the 0dBm requirement for CW interference without performance degradation. However, IFF power is likely to be 500W (3dB less), and antenna rejection is likely to be > 6dB at 1090 MHz.

**L-band Satcom vs IFF:**